

Amendments to the Specification:

Please amend the paragraph starting at page 12, line 5, as follows:

-- The light beam is generated by a light source, for example, a plasma light source or a mercury-vapor lamp. This light beam is at least partially taken up by a condenser optic. The condenser optic includes a first pupil plane wherein a first pupil illumination is generated by the light beam. This first pupil illumination exhibits no ellipticity when the condenser optics include optical components whose optical effects are rotationally symmetrical to the optical axis and when the light source exhibits an emission characteristic rotationally symmetric symmetrical to the optical axis. The emission characteristic is given by the distribution of the ray angles to the optical axis. --

Please amend the paragraph starting at page 17, line 26, as follows:

-- In the following, it will be shown how the use of the diaphragm 201 influences the ellipticity of the pupil illumination. For this purpose, the diaphragm 201 is first removed from the illuminating system 213. In this embodiment, the light arc of the light source 223 has a length of 4 mm and a diameter of 6 mm. The light rays, which are emitted by the light source 223, have an angle of between 60° and 135° with respect to the optical axis OA. The light arc is imaged by the condenser optic 210 on the entry surface 247 and generates a light spot having a maximum diameter of 41 mm which is thereby greater than the rod height by 315%. The rays have a

maximum angle of 18° with reference to the optical axis OA. The diameter of the light spot and the ray angles at the entry surface are dependent upon the position of the zoom lenses and the axicon lenses (233, 235) in the objective 229. In this example, the axicon lenses (233, 235) are closed and the objective 229 has a focal length of 77 mm. The rear focal plane of the objective 229 is close to the location of the second focal point 227 of the ~~mirror 225~~, mirror 225 and the forward focal plane is close to the location of the pupil intermediate plane 243. The focal length of the objective 245 is 90 mm. The rearward focal point is close to the location of the pupil intermediate plane 243 and the forward focal point is close to the location of the diaphragm 201. The rod integrator 211 generates a homogeneous field illumination at its exit surface and this field illumination is imaged by the REMA objective 251 on the ~~mask 217~~ mask 219 carrying structure. Following the field plane with the masking system 249 and after the lens group 253 having the focal length 123 mm, the pupil plane 255 of the REMA objective 251 follows. The pupil illumination is viewed in the pupil plane 255 as intensity distribution $I(x,y)$. The rearward focal plane of the lens group 253 is disposed close to the location of the masking system 249 and the forward focal plane is close to the location of the pupil plane 255. --

Please amend the paragraph starting at page 19, line 29, as follows:

-- With the diaphragm 201, the ellipticity of the pupil illumination is 2.5%. The ellipticity is significantly lower and has a more tolerable value compared to an integrator unit 209 without diaphragm (ellipticity 19%). With the

diaphragm 201, one loses only 32% of the total intensity compared to an integration integrator unit 209 without diaphragm. The in-coupling efficiency of the diaphragm 201 is 14.6%. Compared to a circular diaphragm, the in-coupling efficiency is greater by a factor of 1.45. The total intensity is greater by a factor of 1.3 than for an integrator unit having a circular diaphragm. --